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Experimental and theoretical study of adsorption of L-cysteine on the passivation and corrosion inhibition of aluminum alloy in alkaline environment

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Abstract: L-Cysteine (L-Cyst) was tested as a corrosion inhibitor of 3003 aluminum alloy (AA3003) in Na₂CO₃ 0.1M + NaCl 1M solution. The inhibition action of this inhibitor was studied by using electrochemical impedance spectroscopy (EIS), potentiodynamic polarization (PDP), and cyclic voltammetry (CV) techniques. The temperature effect on the inhibition efficiency was studied in the range from 298 to 328K, and the values of activation thermodynamic parameters were calculated and explained. Experiment results show that inhibition efficiency increases with the increase of L-Cysteine concentration, and its inhibition efficiency reaches 92% at 10^{-3} M. The inhibition efficiency decreases slightly with the elevation of a corrosive medium temperature. Analysis of the polarization curves revealed that L-Cyst is considered a mixed inhibitor. The results from electrochemical measurements and theoretical calculations are in good agreement. The morphological changes of the surface during corrosion, in the presence and absence of the inhibitor, were studied by scanning electron microscopy (SEM).

Keywords: Aluminum Alloy; Corrosion inhibition; PDP; CV; EIS; DFT; L-Cysteine.

1. Introduction

Aluminum is used as packaging in the food industry; in addition, it is oxidizable in a chlorinated alkaline medium; indeed, the choice is justified by this last property.

Corrosion of Aluminum and its alloys has attracted much attention from many researchers due to their high mechanical intensity, low cost, low density, and good machinability. They have been widely used in industrial applications, especially in constructions, electronics, packing, storage, transportation machinery 1-6. Efforts have been equipment, and made to protect the aluminum surface's integrity in an aggressive alkaline medium or another corrosive environment. In recent decades, the addition of inhibitors has been considered the most common approach to hinder Aluminum's corrosion $^{7-10}$. The inhibition of corrosion materials by non-toxic organic inhibitors is an encouraging solution that can effectively replace the usual toxic chemical inhibitors such as azole and thiol compounds ¹¹⁻¹³. Organic inhibitors' mechanism action is explained by physical and/or chemical adsorption on the metal

surface ^{12,14-16}. This inhibitive action depends on the physicochemical properties of the inhibitor atoms, such as the functional group and the aromaticity and the presence of the heteroatoms ^{17–19}, without forgetting the nature of the surface, the temperature, and the pressure of the reaction ²⁰.

Azzouyahar and co-workers investigated the corrosion inhibition of AA3003 in Na_2CO_3 by Nigella Sativa Oil ²¹. The results of this study revealed that Nigella Sativa oil acts as a suitable inhibitor of aluminum corrosion in a solution of 0.1M Na_2CO_3 ; the Inhibition efficiency reaches 91% for 4g. L⁻¹ at 298K.

Barouni et al. tested some amino acid compounds such as Arginine (Arg), Cysteine (Cys), Glycine (Gly), Lysine (Lys), and Valine (Val) on the behavior of copper corrosion in 1M HNO₃²². This study shows that Cys is the best inhibitor of copper corrosion in 1M HNO₃; the inhibition efficiency attains 61% at 10⁻³M.

Chadili et al worked on the inhibition of the corrosion inhibition of Aluminum alloy 3003 in a hydrochloric

acid medium using oil mill liquid by-product (OMW)

*Corresponding author: Said Kharacha Email address: said.kharacha@edu.uiz.ac.ma DOI: http://dx.doi.org/10.13171/mjc02103041563sk Received December 12, 2021 Accepted January 5, 2021 Published March 4, 2021 as an inhibitor. The experimental results reveal that OMW has a good inhibiting effect on the corrosion of AA3003 alloy in the tested solution and acts as a cathodic inhibitor 23 .

The purpose of the present work is to investigate the corrosion inhibition action of L-cysteine named 2-amino-3-mercapto propanoic acid shown in Figure 1 on aluminum alloy's corrosion Na₂CO₃ 0.1M+NaCl 1M solution. The techniques solicited were: Potentiodynamic polarization curves, cyclic voltammetry (CV), and electrochemical impedance spectroscopy (EIS). Effect of inhibitor concentration, the temperature on the corrosion, inhibition, and passivation behavior were thoroughly investigated and discussed. The thermodynamic feasibility of adsorption of the L-Cyst inhibitor molecule on the aluminum surface was also studied. Scanning electron microscopy is used to look at surface morphological changes during polarization studies, with and without inhibitor.

$$\begin{array}{c} H_2 \\ SH-C - HC - C \\ H_1 \\ NH_1 \end{array} OH$$

Figure 1. Chemical structure of L-cysteine

2. Experimental

2.1. Working electrode

The sample used in this study is 3003 aluminum alloy with a chemical composition (wt.%): Si, 0.12, Fe, 0.31, Cu, 0.008, Mn, 1.27, Mg, 0.95, and remainder Al 24 .

The working specimen was cut from the plate, leaving only 0.16 cm² of the surface area exposed to the electrolyte. Before each experiment, the working electrode was mechanically polished with fine grades of emery papers (400 - 1200 grade). Then it was degreased with acetone, washed with double distilled water, and dried before immersing in the corrosion medium. All experiments were performed at different temperatures under the same experimental conditions.

2.2. Corrosive solution

The corrosive medium was $Na_2CO_3 0.1M + NaCl 1M$ solution prepared by dissolving 10.6 g of sodium carbonate and 58.44 g of sodium chloride in 1000 mL of double-distilled water. The solution tests are freshly prepared before each experiment. The inhibitor's concentration range was 10^{-3} to $10^{-6}M$. All electrochemical tests have been performed in aerated solution at pH=11.

2.3. Electrochemical techniques

Electrochemical measurements were carried out by using an electrochemical workstation, versa STAT 3 potentiostat piloted by versa studio software. The arrangement used was a conventional three-electrode compartment glass cell with a platinum counter electrode and a saturated calomel electrode (SCE) as reference. The working electrode was made of aluminum alloy (AA3003). All the values of potential are referred to the SCE. The polarization studies were carried out immediately after the EIS studies on the same electrode without further surface treatment.

2.3.1. Potentiodynamic polarization studies

Finely polished aluminum alloy specimen was exposed to the corrosion medium of Na_2CO_3 0.1M+NaCl 1M solution in the presence and absence of the inhibitor at different temperatures (298 – 328K) and allowed to establish a steady-state open circuit potential (OCP).

The potentiodynamic current- potential curves were recorded by polarizing the specimen from - 1800 mV to 0 mV at a scan rate of 1 mV.s⁻¹.

2.3.2. Electrochemical impedance spectroscopy studies (EIS)

The impedance measurements were carried out in the frequency range of 10 kHz to 0.1 Hz, at the OCP, by applying 10 mV wave AC voltage. The double-layer capacitance (C_{dl}) and the charge transfer resistance (R_{ct}) were calculated from the Nyquist or Bode plots.

At least three similar results were considered in all the above measurements, and their average values are reported.

2.4. Scanning Electron Microscope (SEM)

The aluminum alloy's surface morphologies immersed in Na_2CO_3 0.1M+NaCl 1M solution for 20days with and without the inhibitor L-Cyst were observed via SEM (TESCAN VEGA 3) at an accelerating voltage of 20 kV.

2.5. Quantum Chemical Calculation

The quantum theoretical calculations were carried out with the Gaussian 03 program package ²⁵. The complete geometry optimization of the undertaken MTP as corrosion inhibitor was carried out at DFT (Density Functional Theory) using the hybrid functional B3LYP level taking into account the exchange and the correlation with Beck's three parameters exchange functional along with Lee and al. non-local correlation functional ^{26,27}. All Calculations of DFT/B3LYP theory were done using 6-31G (d,p) basis set. This approach is widely utilized in the analysis of the characteristics of the corrosion process. The following quantum chemical parameters were evaluated from the optimized molecular structure: the dipole moment (μ) , the energy of the highest occupied molecular orbital (E_{HOMO}), the energy of the lowest unoccupied molecular orbital (E_{LUMO}), the energy band gap ($\Delta E_{gap} = E_{HOMO} - E_{LUMO}$), the electron affinity (A) (the ionization potential (I) and the number of transferred electrons (ΔN).

3. Results and Discussion

3.1. OCP measurement

OCP measurement is a simple additional tool that provides complementary information to EIS results regarding the corrosion undergone by the AA3003 after exposure to aggressive solutions ²⁸. Before each polarization manipulation or EIS, the working electrodes were immersed in Na₂CO₃ 0.1M+NaCl 1M solution for 30 min to access the free corrosion potential or the quasi-stationary E_{ocp} value. The plots of E_{ocp} vs time of AA3003 in the absence and presence of inhibitor are given in Figure 2.

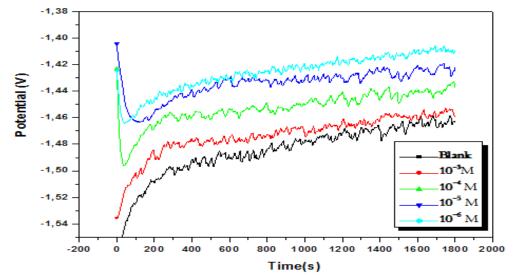


Figure 2. OCP plots for AA3003 in Na₂CO₃ 0.1M+NaCl 1M containing L-Cyst at different concentrations

The OCP is the potential of the working electrode concerning reference electrode without applied any potential or current. It is required to maintain the stability of OCP before running the polarization and EIS experiments. Figure 2 shows the variation of OCP of working electrode with time in uninhibited and inhibited system at 298K.

In the presence of L-Cyst, the potential has been evaluated towards higher values. The potential stabilizes towards the value -1440 mV / ECS, after which the potential begins to decrease with the increase of the immersion time. Translates the system's instability, whereas for aluminum one observes a rather regular decay that would indicate weak protection of the natural film of alumina.

3.2. Behavior of AA3003 in alkaline medium

Figure 3 shows the potentiodynamic polarization curve of AA3003 in an alkaline solution. In the cathodic domain, Tafel behavior characterized by linear regions in the proximity of the potential of corrosion indicates that the process of reduction of the water is an activation control ²⁹⁻³¹:

$$2 H_2 O + 2 e^- \longrightarrow 2 OH^- + H_2$$
 (1)

Examination of the anode curve shows that AA3003 exhibits a passivation phenomenon with rupture of passivity. Indeed, starting from OCP, the anodic current density increases with the electrode potential to reach the passivation stage. In this stage, the anodic current density is almost constant, and nomad passivation current density I_{pass} . This phenomenon is probably attributed to the formation of a passive film on the AA3003 surface. When the anodic current density increases abruptly, the pitting potential E_{pit} is reached.

The following reaction mechanism can represent the dissolution of the metal:

$$Al^{3+} + 3 OH^{-} \longrightarrow Al(OH)_{3} + 3 e^{-} (2)$$

$$Al(OH)_3 + OH \longrightarrow Al(OH)_4^-$$
 (3)

At alkaline pH the aluminum hydroxide dissolves to give the ion AlO_2^- very soluble according to the reaction balance ³²:

$$Al(OH)_4^- \longrightarrow AlO_2^- + 2H_2O$$
 (4)

The Nyquist diagram is presented in Figure 4. calculated from the difference between the reel impedance value at high frequency and their value at a low frequency of loop (loop diameter). The semicircle loop indicates that a charge transfer process mainly controls the corrosion of aluminum alloy.

3.3. Effect of L-Cyst concentration 3.3.1. Potentiodynamic Polarization Curves

The effect of L-Cyst was studied using potentiodynamic polarization curves. Figure 3 shows the obtained results of AA3003 in Na₂CO₃ 0.1M+NaCl 1M solution in the absence and presence of a tested compound at different concentrations.

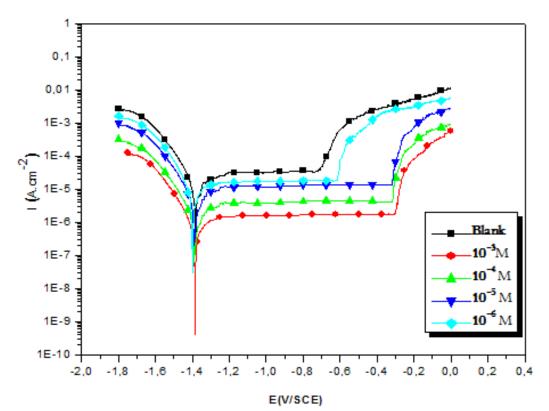


Figure 3. Polarization curves for AA3003 in Na₂CO₃ 0.1M+NaCl 1M solution with and without L-Cyst at different concentrations (T=298K)

The polarization curves show the reactions of the anodic and current density was slowed with the addition of tested compound for all envisaged concentrations. Generally, the organic inhibitors acted by physical or chemical adsorption or both on the metal's surface. The slowdown of reactions, anodic and cathodic, is marked by the rise of concentration inhibitors. The corrosion parameters, including corrosion potential (E_{corr}), current density (I_{corr}), cathodic Tafel slope (β_c), passivation current density (I_{pass}), pitting potential (E_{pit}) and inhibition efficiency (E_I %) are listed in Table 1.

The shape of the cathodic and anodic curves is not changed. It is found that I_{pass} decreases with the increase of the inhibitory concentration to reach a value of $3\mu A / cm^2$ for a concentration of 10^{-3} M.

 ΔE being the difference between E_{pit} and E_{corr} ($\Delta E = E_{pit} - E_{corr}$), from the results obtained, we find that ΔE increases with the concentration of the inhibitor. However, E_{pit} moves towards positive values. We can say that this type of inhibitor is effective for passive materials.

No effective change was observed in the corrosion potential (E_{corr}) value concerning the blank. Both anodic and cathodic polarization is influenced simultaneously, almost to the same extent, which indicates L-Cyst's influence on both the anodic and the cathodic reactions, water reduction, and metal dissolution. If the corrosion potential displacement is

more than 85mV for the blank's corrosion potential, the inhibitor can be seen as a cathodic or anodic type 33 . However, in the present case, the maximum displacement in E_{corr} is 24mV which is much less than 85mV, suggesting a mixed inhibitor mode.

The inhibition efficiency is calculated following the relationship:

$$\mathbf{E}_{\mathbf{I}}\% = \frac{\mathbf{I}_{corr} - \mathbf{I}_{corr}'}{\mathbf{I}_{corr}} \times \mathbf{100}$$
(1)

Where, I_{corr} and I'_{corr} are the corrosion current density values without and with the inhibitor, respectively. We noted that I_{corr} and I'_{corr} were determined by extrapolation of cathodic Tafel lines to the corrosion potential.

Table 1 shows that when more inhibitors were added into the corrosive solution, the corrosion current density decreased, and the inhibition efficiency increased.

The results show that in the inhibitor's presence, the corrosion rate is considerably decreased, justifying by the decrease the intensity of corrosion current. For instance, for the curve before adding L-Cyst to the corrosive medium (Na₂CO₃ 0.1M + NaCl 1M), the corrosion current density was 142 μ A/cm², and it was considerably reduced to 13 μ A/cm² for L-Cyst at10⁻³M. and the other hand, observing that the current density is decreased in both cathodic and anodic branches (Figure 3).

Inhibitor	Conc (M)	-E _{corr} (mV/SCE)	I _{pass} (µA cm ⁻²)	E _{pit} (mV/SCE)	$\Delta E = E_{pit}$ E_{corr} (mV/SCE)	$-\beta_c$ (mV dec ⁻¹)	I _{corr} (μA cm ⁻²)	E _I (%)
Blank	-	1379	34	-725	654	133	142	-
L-Cyst	10-3	1437	4	-151	1286	194	13	91
	10-4	1441	5	-275	1166	185	19	87
	10-5	1378	6	-312	1066	194	36	75
	10-6	1412	23	-429	983	198	67	53

Table 1. Polarization parameters of AA3003 in Na₂CO₃ 0.1M+NaCl 1M at 298 K in the absence and presence of L-Cyst.

3.3.2. Cyclic voltammetry measurements cyclic potentiodynamic polarization

Cyclic voltammetry technic was performed in the solution in the absence and presence of the inhibitor, with the potential (E) swept linearly from -1.8 V/SCE

to +0 V/SCE at a sweep rate of 1 mV.s⁻¹. Figure 4 illustrates the cyclic voltammetry curves of aluminum alloy in Na₂CO₃ 0.1M+NaCl 1M medium with and without inhibitor.

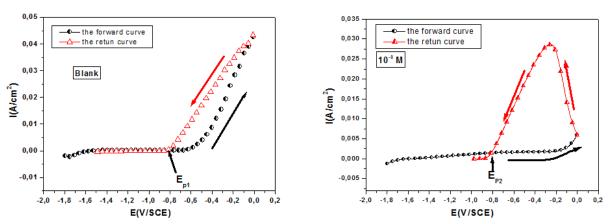


Figure 4. Cyclic voltammetry curves for AA3003 in Na₂CO₃ 0.1M+NaCl 1M solution in the presence and absence of L-Cyst at pH=11 and T=298K

The aluminum alloy presents a passivation phenomenon with a breakdown of passivity (Figure 4) in L-Cyst inhibitor's absence and presence. It is clear from Figure 4 that the pitting potential E_{pit} is modified by addition of the concentration of the inhibitor; in fact, this addition causes a displacement of E_{pit} towards the noblest values and the passive current density I_{pass} decreases with increasing inhibitor concentration.

3.3.3. Electrochemical Impedance Spectroscopy measurements

Figure 5 represents the Nyquist plots for AA3003 in the absence and presence of L-Cyst in Na₂CO₃ 0.1M+NaCl 1M at 298K. It can be observed that all the impedance spectra obtained display one single depressed semicircle, which indicates that the corrosion process is related to the charge transfer process ^{34,35}. The depression in Nyquist semicircles may be due to frequency dispersion, inhomogeneities, and roughness of the metal surface and substance transmission actions ^{36,37}. The similarity in the shapes of Nyquist plots in the absence and presence of inhibitor reveals that the corrosion mechanism is unaffected by the L-Cyst addition. Furthermore, the diameter of the semicircles in L-Cyst's presence is significantly larger than observed in uninhibited solution and increases with increasing inhibitor concentration, which may be due to the formation of protective film on aluminum alloy surface and consequently reduction in corrosion rate ³⁸.

Accordingly, the *EIS* data are simulated by the proposed equivalent circuit presented in Figure 5³⁹. Rs, the solution resistance, Rct denotes the charge-transfer resistance and CPE is a constant phase element. The introduction of CPE into the circuit was necessitated to explain the depression of the capacitance semicircle, which corresponds to surface heterogeneity resulting from surface roughness, impurities, and adsorption of inhibitors. The impedance parameters obtained are reported in Table 2. It has been seen that R_{ct} increased with an increase in inhibitor concentrations. This can be attributed to the formation of an isolating protective film at the metal/solution interface ⁴⁰. The CPE impedance is calculated using the Equation (2):

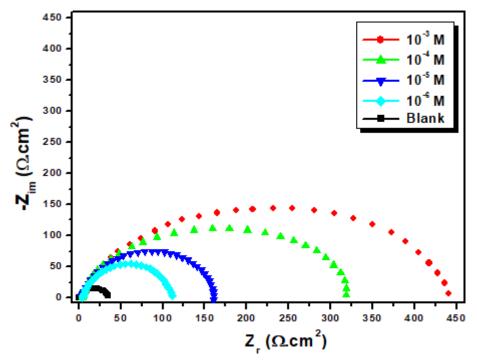


Figure 5. Nyquist plots for AA3003 in Na₂CO₃ 0.1M+NaCl 1M containing different concentrations of L-Cyst

$$\boldsymbol{Z}_{CPE} = \frac{1}{\boldsymbol{Q}_{\cdot}(\boldsymbol{J}\boldsymbol{\omega})^n} \tag{2}$$

Where Q is the CPE constant (in Ω^{-1} ×Sn×cm⁻²), ω is the angular frequency (in rad.s⁻¹), $j^2 = -1$ is the imaginary number, and *n* is a CPE exponent which can be used as a gauge for the heterogeneity or roughness of the surface. In addition, the double layer capacitances, *C*_{dl}, for a circuit including a CPE were calculated by using the following Equation (3) ⁴¹:

$$\boldsymbol{C}_{dl} = \sqrt[n]{\boldsymbol{Q}} \cdot \boldsymbol{R}_{t}^{1-n}$$
(3)

The inhibition efficiency is calculated from the R_{ct} values using the following Equation (4):

$$E_{Rct}\% = \frac{(R'_{ct} - R_{ct})}{R'_{ct}} \times 100$$
 (4)

Where R_{ct} and R'_{ct} are the charge transfer resistance values without and with inhibitor, respectively.

The corrosion of aluminum alloy in Na_2CO_3 0.1M+NaCl 1M is clearly inhibited in the inhibitor's presence and the impedance response change with the increase in inhibitor concentration. The quantitative analysis of electrochemical impedance (EIS) spectra was studied on the basis of a physical model characterizing the charge transfer process at the metal/solution interface. The simplest model includes the charge transfer resistance (R_{ct}) in parallel to the capacitance (C_{dl}) connected with the solution resistance (R_s) (Figure 6). The experimental and theoretical results are in good agreement according to the feting carried out by Zview (Figure 7).

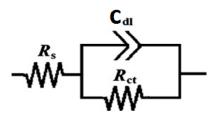


Figure 6. Equivalent electrical circuit corresponding to the corrosion process on aluminum alloy in Na₂CO₃ 0.1M+NaCl 1M

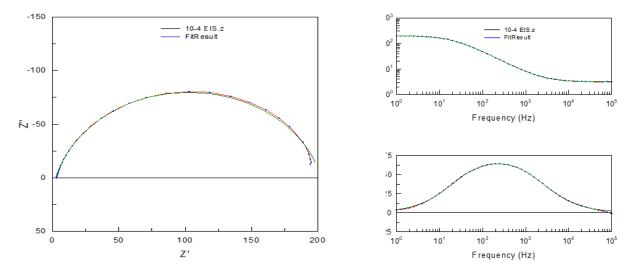


Figure 7. EIS Nyquist and Bode plots for AA3003 in Na₂CO₃ 0.1M+NaCl 1M of L-Cyt

Table 2. Electrochemical Impedance Spectroscopy for corrosion of aluminum alloy in Na₂CO₃ 0.1M+NaCl 1M at various concentrations of L-Cyst.

	Concentration (M)	$R_{\rm ct}$ ($\Omega \times {\rm cm}^2$)	n	Q×10 ⁻⁴ (Ω ⁻¹ .Sn.cm ⁻²)	C _{dl} (µF/cm ²)	E _{Rct} (%)	θ
Blank	-	35	0.85	0.16	4,37	-	-
	10 ⁻³	437.5	0.76	0.304	8	92	0.92
TOA	10-4	318	0.74	0.480	11	89	0.823
L-Cyst	10 ⁻⁵	196	0.75	0.863	22	78	0.734
	10-6	11	0.78	1.42	44	56	0.562

Table 2 shows that the charge transfer resistance (Rct) increases with the increase of inhibitor concentration. However, double layer capacitance (Cdl) decreases because it depends inversely of charge transfer resistance in all concentrations. This result may be attributed to forming a protective layer on the electrode surface 42 .

The results show that the L-Cyst inhibits the corrosion of aluminum alloy in Na2CO3 0.1M+NaCl 1M solution at different concentrations studied. The efficiency increases with the rise of concentration at 298K (Table 2). The $I_E(\%)$ obtained from EIS techniques and those calculated from polarization curves are in good agreement.

3.3.4. Adsorption isotherm and thermodynamic parameters

An inhibitor's action in the alkaline medium is assumed to be due to its adsorption to the metal/solution interface. The kind of adsorption isotherm can give more information about the properties of the studied extracts. Several adsorption isotherms were tested, and the Langmuir adsorption isotherm was found to furnish the best description of the studied organic compound's adsorption behavior. The Langmuir isotherm is given by the following Equation 43 :

$$\frac{C_{inh}}{\theta} = \frac{1}{K_{ads}} + C_{inh}$$
(5)

Where θ is the surface coverage, K_{ads} is the adsorption-desorption equilibrium constant, C_{inh} is the concentration of inhibitor.

Figure 8 shows C_{inh} / θ versus C_{inh} and the expected linear relationship is obtained for this compound. The strong correlation ($R^2 = 0.9999$ for the compound L-Cyst) confirms the validity of this approach. The thermodynamic parameters from the Langmuir adsorption isotherm are listed in Table 3, together with the value of the Gibbs free energy of adsorption ΔG^0_{ads} calculated from the Equation:

$$\Delta \mathbf{G}_{ads}^{0} = -\mathbf{RT} \ln(\mathbf{55}, \mathbf{5} \times \mathbf{K}_{ads}) \tag{6}$$

Where 55.5 is the concentration of water, R $(8.314 \text{ J.K}^{-1}.\text{mol}^{-1})$ is the universal gas constant and T is the absolute temperature (K), K_{ads} the adsorption–desorption equilibrium constant ⁴⁴.

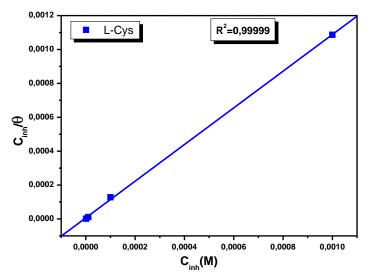


Figure 8. Langmuir adsorption of inhibitor on the aluminum surface in 0.1 M Na₂CO₃+NaCl 1M solution at 298K

Table 3. Adsorption parameters of inhibitor for aluminum alloy in 0.1 M Na₂CO₃+NaCl 1M solution at 298K.

Inhibitor	Slope	Slope K _{ads} (M ⁻¹)		ΔG_{ads}° (kJ/mol)	
L-Cyst	1.1444	564971.75	0.9999	-42.74	

The ΔG^0_{ads} value is calculated as -42.74 kJ. mol⁻¹ for L-Cyst. In the literature, if the absolute values of ΔG^0_{ads} are less than 20 kJ.mol⁻¹ consistent with the electrostatic interaction between the charged metal and charged molecules (physisorption). But if those more than 40 kJ.mol⁻¹ involve sharing or transferring electrons from the inhibitor compound to the metal surface to form a coordinate type of bond (chemisorption) ^{45,46}. The standard adsorption free energy value shown in Table 3 suggests that adsorption is chemisorption.

3.4. Effect of temperature

The effect of temperature on the corrosion rate of aluminum alloy in 0.1 M Na₂CO₃+NaCl 1M with the addition of the L-Cyst inhibitor is made from 298 to 328K shown in Table 4 using electrochemical

impedance spectroscopy measurements technique. R_{ct} decrease with increasing temperature both in uninhibited and inhibited solutions, and the efficiency of inhibition by L-Cyst decreases slightly with increasing temperature. The results confirm that the L-Cyst acts as an efficient inhibitor in the range of temperature studied.

On the other hand, the values of R_{ct} were employed to calculate values of the corrosion current density (I_{corr}) at various temperatures in the absence and presence of L-Cyst using the following Equation ⁴⁷:

$$I_{corr} = R.T(Z.F.R_{ct})^{-1}$$
⁽⁷⁾

R is the universal gas constant, T is the absolute temperature, z is the valence of Aluminum (z = 3), F is the Faraday constant (F = 96485 Coulomb) R_{ct} is the charge transfer resistance.

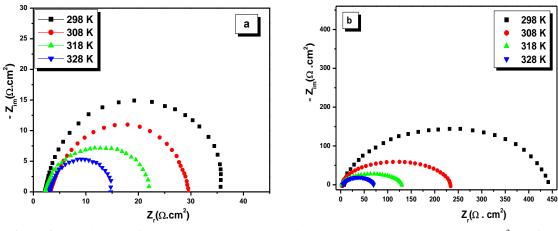


Figure 9. Nyquist plots for corrosion aluminum alloy in 0.1 M Na₂CO₃+NaCl 1M (a) and 10⁻³ M of L-Cyst (b) at different temperatures

	Temperature (K)	$\frac{R_{\rm ct}}{(\Omega\times{\rm cm}^2)}$	п	Q×10 ⁻⁴ (Ω ⁻¹ .Sn.cm ⁻²)	C_{dl} (μ F/cm ²)	η _{EIS} (%)	θ
	298	35	0.89	0.39	101	-	-
D1 1	308	28	0.87	0.54	57	-	-
Blank	318	22	0.85	0.79	48	-	-
	328	14	0.84	0.98	38	-	-
	298	437,5	0.76	0.304	8	92	0.92
L-Cyst	308	233	0.77	0.312	7	88	0.88
10 ⁻³ M	318	129	0.74	0.482	8	83	0.83
	328	70	0.72	0.655	7.5	80	0.80

Table 4. Effect of temperature on the aluminum alloy corrosion in 0.1 M Na₂CO₃+NaCl 1M and at 10^{-3} M of L-Cyst.

The logarithm of the corrosion rate of aluminum alloy I_{corr} can be represented as a straight-line function of 1000/T (Arrhenius equation, Figures 12-13).

$$I_{corr} = A. exp(-\frac{E_a}{PT})$$
(8)

Where A is Arrhenius factor, E_a is the apparent activation corrosion energy ((J/mol), R is the perfect gas constant (8.314 J.K⁻¹.mol⁻¹), and T the absolute temperature (K).

The value of E_a can be calculated from the slope of the straight line of Arrhenius plots. The higher value of E_a in L-Cyst's presence than its absence indicates strong inhibitive action of the organic compound by increasing the energy barrier for the corrosion process ⁴⁸.

However, the adsorption phenomenon has been successfully explained by thermodynamic parameters. To elucidate the inhibitors' properties further, the kinetic model was another useful tool to explain the mechanism of corrosion inhibition for the inhibitor. The activation parameters for the corrosion process were calculated from the Arrhenius equation:

$$I_{corr} = \frac{RT}{Nh} \cdot \exp\left(\frac{\Delta S_a}{RT}\right) \cdot \exp\left(-\frac{\Delta H_a}{RT}\right)$$
(9)

Where h is Planck's constant, N Avogadro's number (mol⁻¹), R the universal gas constant, ΔH_a the activation enthalpy (J/mol), and ΔS_a is the activation entropy(J/mol).

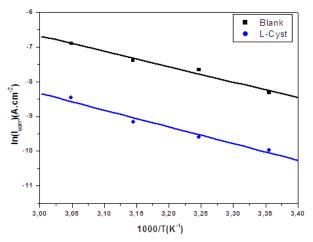


Figure 10. Arrhenius plots of aluminum corrosion in 0.1 M Na₂CO₃+NaCl 1M with and without inhibitor (10^{-3} M)

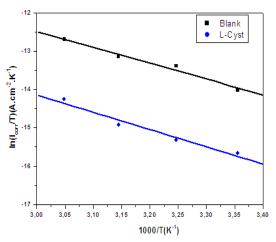


Figure 11. Relation between Ln (I_{corr}/T) and 1000/T at different temperatures (10⁻³ M)

Table 5. The value of activation parameters E_a , ΔH_a and ΔS_a for AA3003 in 0.1 M Na₂CO₃+NaCl 1M in the absence and presence of L-Cyst at 10⁻³ M.

Inhibitor	$\Delta H_a(kJ/mol)$	$\Delta S_a (J/mol)$	E _a (kJ/mol)	Ea-ΔH _a	
Blank	24.15	-229.93	26.75	2.60	
L-Cyst	37.43	-210.45	39.87	2.60	

The increase of ΔS_a is usually interpreted as an increase in disorder as the reactants are converted to the activated complexes ⁴⁴. From Table 5, we note that a less harmful value of ΔS_a is obtained in the presence of L-Cyst, while a more negative value is observed in the uninhibited solution. The values of ΔS_a calculated in the fact of inhibitor decrease compared with the blank solution. This result is interpreted as an increase in disorder ⁴⁷.

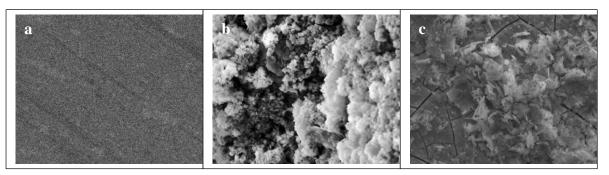
The difference between the two values is almost constant with an average value of 2.60 kJ.mol⁻¹ which is very close to the average value of the product (RT) in the investigated temperature range. Such behavior is characteristic of a unimolecular gas-phase reaction obeying the following Equation ⁴⁹:

$$\boldsymbol{E}_{\boldsymbol{a}} - \Delta \boldsymbol{H}_{\boldsymbol{a}} = \boldsymbol{R}\boldsymbol{T} \tag{10}$$

3.5. SEM studies

SEM technique was employed to prove L-Cyst's corrosion resistance ability further, and the surface

observation images of the aluminum alloy after a 20 days exposure in 0.1 M Na₂CO₃+NaCl 1M solution without and with inhibitor are shown in Figure 6. Before immersion, the bare aluminum plate looks very smooth (Figure 12a). In contrast, in the absence of an inhibitor, the AA3003 presented a very rough surface covered with a vast amount of deep cracks and large holes, suggesting severe damage and painful dissolution of aluminum alloy in contact with an aggressive solution (Figure 12b). Nevertheless, in Figure 12c, aluminum alloy's dissolution rate was substantially inhibited by L-Cyst, exhibiting a comparatively smooth surface with a few small pits. Therefore, it is concluded that the regular distribution of the L-Cyst. Consequently, it is concluded that the regular distribution of L-Cyst molecules adsorbed on the AA3003 surface generates coherent protective layers, which effectively prevent Cl⁻ ions from penetrating.



3.6. DFT Calculation results

The quantum chemical calculations are used to make sure the relationship between the inhibition effect of the synthesized inhibitor and its molecular structures. The optimized molecular structure and the frontier molecular orbitals density distributions are shown in Figure 13. The quantum chemical parameters are regrouped in Table 6.

Table 6. Calculated quantum chemical parameters of the inhibitor molecule.

Model	E _{HOMO} (eV)	E _{LUMO} (eV)	ΔE (eV)	μ (D)	η (eV)	σ (eV ⁻¹)	χ (eV)	ΔΝ
B3LYP	-6.530	-0.170	6.360	4.932	3.180	0.314	3.350	0.15

According to Koopman's theorem ⁵⁰, the energies of HOMO and LUMO are correlated to the ionization potential (I) and the electron affinity (A), respectively, which defined as follows:

$$I = -E_{HOMO}$$
(11)

$$A = -E_{LUMO}$$
(12)

The energy gap is determined as follow:

$$\Delta E = E_{LUMO} - E_{HOMO} \tag{13}$$

The values of I and A were considered for the calculation of the electronegativity χ and the global hardness η was determined using the following equations:

$$\chi = \frac{I+A}{2} \tag{14}$$

$$\eta = \frac{I-A}{2} \tag{15}$$

The fraction of electrons transferred from inhibitor to metal surface (ΔN) was estimated according to Pearson ⁵¹.

$$\Delta N = \frac{\chi_M - \chi_{inh}}{2.(\eta_M + \eta_{inh})} = \frac{\phi_M - \chi_{inh}}{2\eta_{inh}}$$
(16)

Where (χ_M, η_M) and (χ_{inh}, η_{inh}) are, respectively, the electronegativity and hardness of the metal and the inhibitor when ϕ_M is the work function. In our study, the theoretical values of electronegativity $\phi_{Al} = 4.28 \text{eV}^{51}$ and hardness $\eta_{Al} = 0^{52}$ have been used for Aluminum.

Generally, the inhibition efficiency increases with the increase in electron-donating ability to the metal surface.

According to Lukovits's study, this is true if $\Delta N < 3.6^{53}$. Based on these calculations, we can say that our inhibitor favors chemical adsorption on the aluminum alloy surface.

In this paper, the HOMO and LUMO orbital energies were calculated by using the B3LYP method with 6-31G. All other calculations were performed using

the results with some assumptions. The higher values of E_{HOMO} indicate an increase for the electron donor, which means a better inhibitory activity with increasing adsorption of the inhibitor on a metal surface. In contrast, E_{LUMO} suggests the ability to accept the electron of the molecule. The inhibitor's adsorption ability to the metal surface increases with the increasing of E_{HOMO} and decreasing of E_{LUMO} .

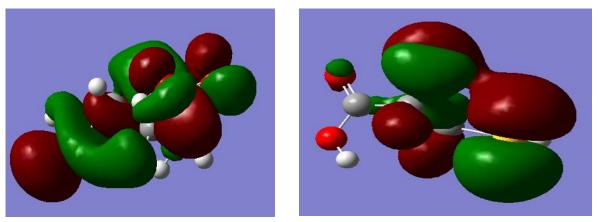


Figure 13. The frontier molecular orbital density distribution of L-Cyst (left, LUMO; right, HOMO)

4. Conclusion

The organic compound L-Cyst as corrosion inhibitor for aluminum alloy in a 0.1 M Na₂CO₃+NaCl 1M solution was investigated. Through the results from our experimental study, we quote the following conclusions:

- For L-Cyst, their inhibition efficiency increased with increases in inhibitor concentration, and they belonged to mixed-type inhibitor predominantly retarding the cathodic reaction.
- The inhibiting efficiencies determined by methods potentiodynamic polarization testing and EIS measurements are all in good agreement.
- The adsorption processes of L-Cyst molecules followed the Langmuir adsorption isotherm. The calculated ΔG°_{ads} values indicated that this inhibitor was spontaneously absorbed on the aluminum alloy surface and was more inclined to a chemisorption mechanism at 298K.
- The surface morphologies images were suitable proof for reducing the dissolution of aluminum alloy ascribed to the formation of protective L-Cyst film on the metal surface.

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